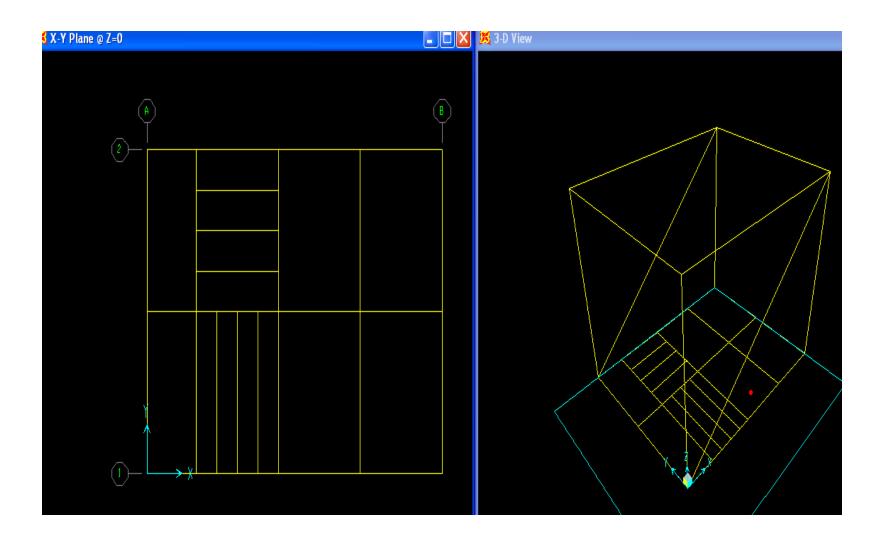
Heavier equipment with faster machine speeds coupled with higher costs have made rule-of-thumb approaches and "rigid structure" assumptions either unsafe or too conservative for the design of many structures with vibrating machinery. SAP2000 can easily compute natural frequencies, deformations and forces in the structure with consideration of structure mass and flexibility. Using less rigorous design approaches, these factors are either ignored, conservatively assumed, or handled in a simplified approximate fashion. Sizing and design of a skid or foundation supporting vibrating equipment is beyond the scope of this tutorial. However, here are a few considerations:

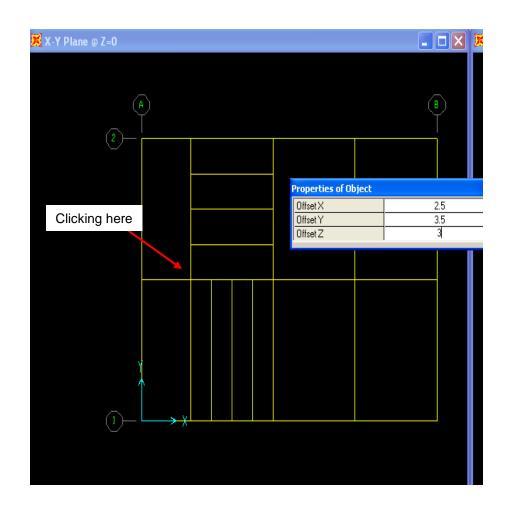
- Run multiple analyses which vary soil spring constants and damping ratio to account for uncertainties of soil data.
- Acting frequency of the vibrating machinery should not be close to the structure's resonant frequency
- Dynamic effects to and from adjoining structures and equipment. Modular skids may be designed in isolation for vibrating equipment. Yet these skids can be added to other parts of a larger structure which may change the initial design assumptions.

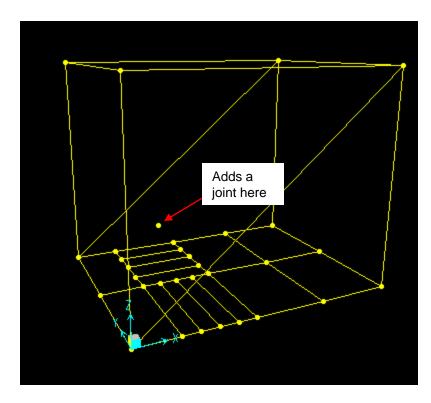


Use SAP2000's "Draw special joint" to add joints at the Center of Mass (CoM) for each piece of vibrating equipment and also at the centroid of unbalanced load locations. CoM can be referred to as Center of Gravity in this context. In many cases, the vendor will give separate CoM locations for major components (pump, gearbox, turbine, turbine rotor, generator, etc.), in which case you would add joints for each component of the equipment where you will assign force/weight which will be converted to mass. In addition, you need to draw a joint at each unbalanced load location. In this example, we'll take a simplified modeling approach by lumping each equipment CoM at just 1 joint location per machine.

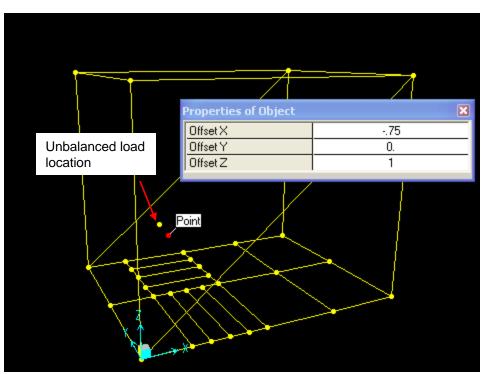


'Draw special joint' tool adds a joint offset in current units (units displayed bottom right portion of the SAP2000 screen) from wherever you mouse click in the model. In this example, we use ft. units modeling the CoM and unbalanced load location for two pieces of equipment. Use 'Draw special joint' button on the toolbar or find it in the Draw menu.

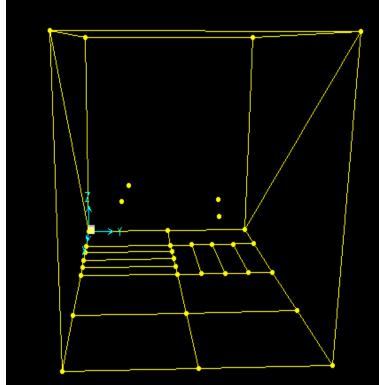




Assuming the 1st special joint was the machine CoM, we'll draw another special joint to specify the centroid of unbalanced load by adjusting offsets and then clicking the CoM joint to specify the unbalanced load location, In this fictitious example, the unbalanced load is positioned 1 ft. above and -.75 ft Y from the CoM. Using the same Draw tool, we add 2 more joints on the other side based on vendor specified CoM and unbalanced load location. Dimensions for this example are not important, because each project will be different. At this point we have 4 joints offset from the structure which need to be connected to the structure.

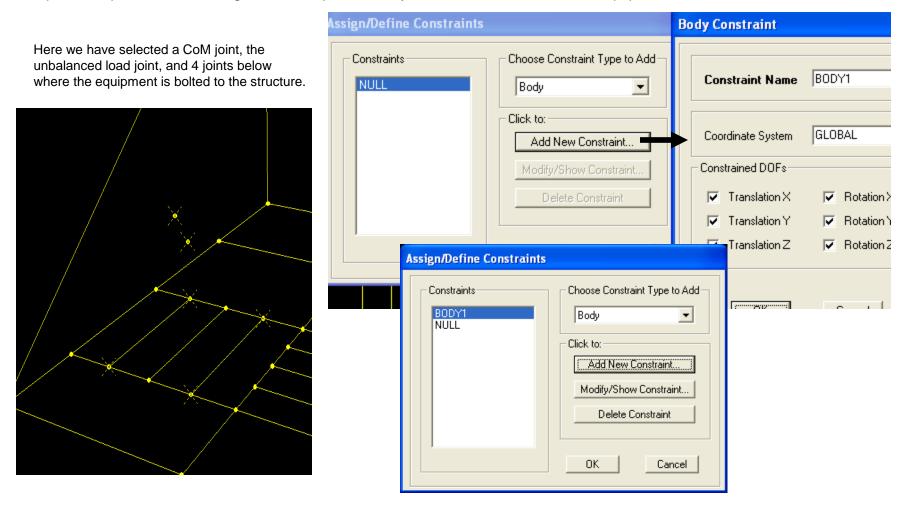


4 joints offset from structure

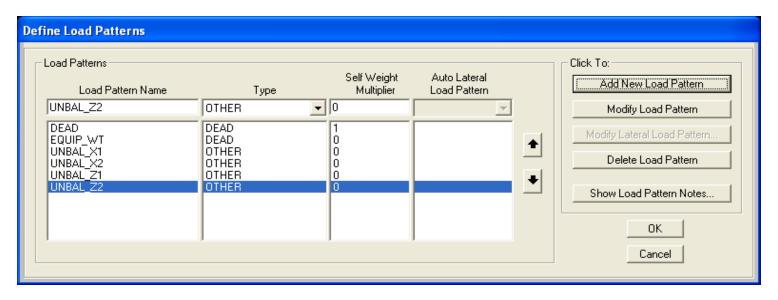


Connect the CoM and unbalanced load joint of each piece of equipment to the structure by selecting the CoM and unbalanced load joints of one machine along with connection points where the equipment is bolted or welded to the structure, then use Assign menu>Joint>Constraints using Body type of constraint as shown below. Body joint constraints rigidly link the selected joints together while considering the moment differentials from their offset distances. Joint Constraints are preferable to rigid "dummy" frame members because overly rigid elements relative to the stiffness of what they are connecting to can introduce analytical problems, particularly in dynamic analysis. Constraints avoid these potential numerical instabilities. If there were multiple CoM's for a particular machine representing various components, you would select all CoM's for the machine when assigning a constraint to the structure.

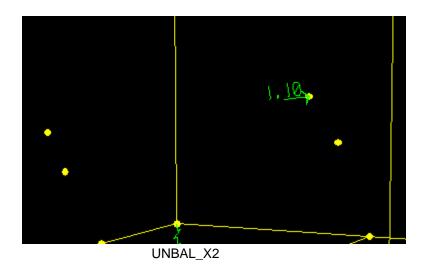
Repeat this procedure to assign a new, separate Body constraint, BODY2, to the equipment on the other side.

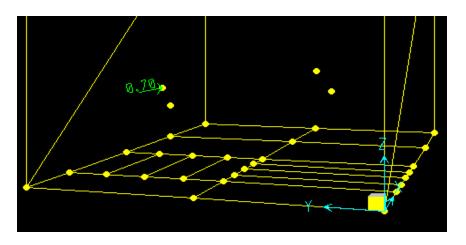


Under Define>Load Patterns, add load patterns for equipment CoM and max unbalanced loads. You can assign the CoM (weight) of the equipment all to one load pattern, or alternatively create separate load patterns for each equipment weight. Since the unbalanced loads will vary in both magnitude and machine speed, you would define separate load patterns for each unbalanced load assignment. We will next assign max unbalanced load in the X and Z directions for each piece equipment, .7 Kip unbalanced joint load in each direction for one machine and 1.1 Kip unbalanced joint load for the other machine.



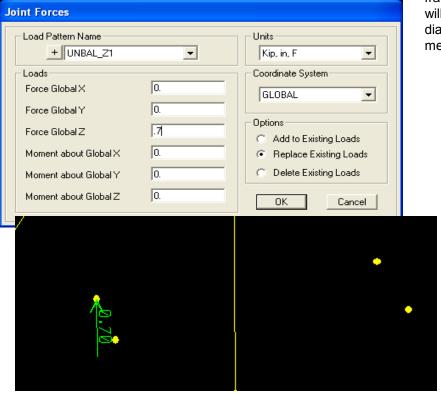
Select joints, one at a time, and assign X direction unbalanced load to their respective load patterns



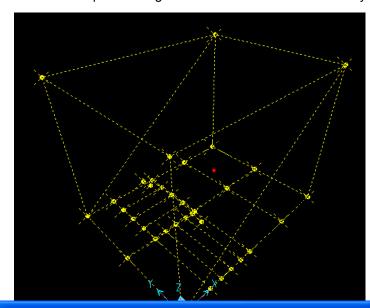


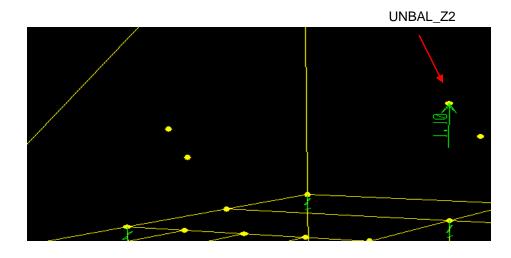
UNBAL X1

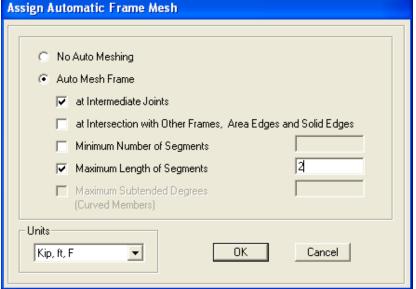
Next, assign unbalanced loads in Z direction



Select all, then Assign menu>Frame>Automatic Frame mesh and specify that frames be automatically divided for internal analysis with a max length of 2 ft. This will only affect internal analysis. Each frame element will display 1 moment diagram and be designed using it's physical length. For dynamic analysis, meshing can affect results. It's up to the engineer to determine mesh sensitivity.

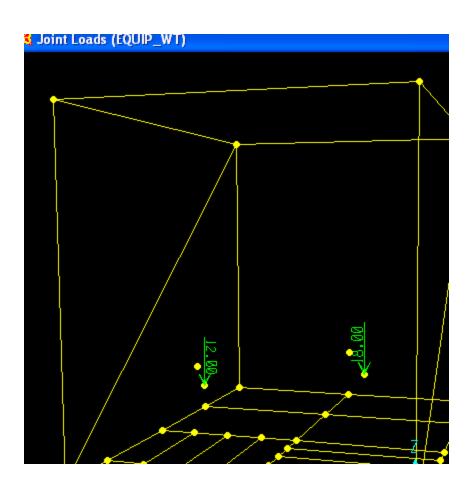






We assign CoM (weight) loads for each piece of equipment. In this example, a 12 Kip weight load for one piece of equipment and an 18 Kip weight load for the other equipment, assigning them both under the EQUIP_WT load pattern.

This is a simplified model which considers only the vibrating equipment. But if there were other stationary equipment or piping or anything else with significant mass that will be on this structure along with the vibrating equipment, those items would need to be modeled using loads, or modeled explicitly with elements.



Using Define menu>Functions>Time history, define sine and cosine functions based on machines speeds. In this

Choose Function Type to Add

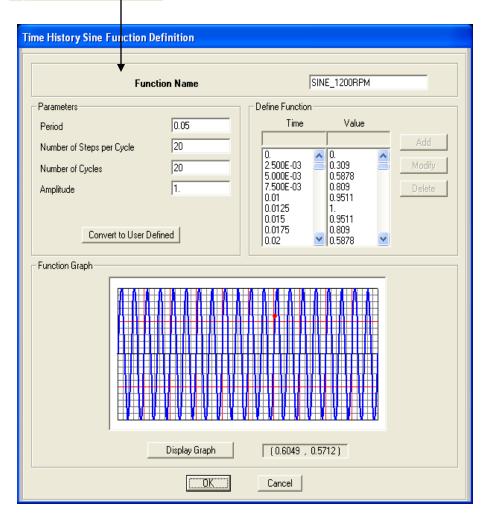
Sine

Click to:

Add New Function...

example we'll analyze one machine running at 1200rpm while the other is running at 1800rpm. Use the Sine and Cosine function types to help you quickly define functions. Period of 1200 rpm is .05. Period of 1800 rpm is .0333. Because we are going to run a "periodic" time history dynamic analysis, we do not have to define many cycles in order to avoid transient startup "spike" in results. 20 cycles should be plenty.

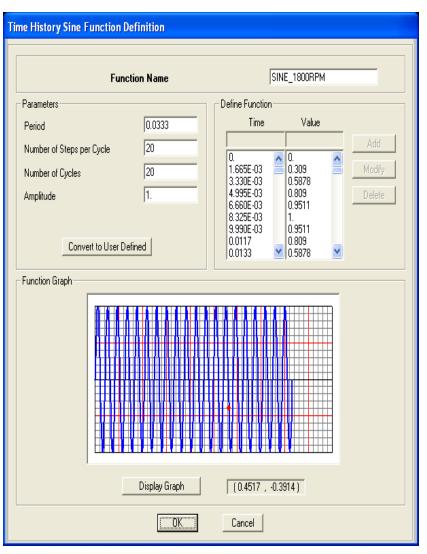
Cosine function

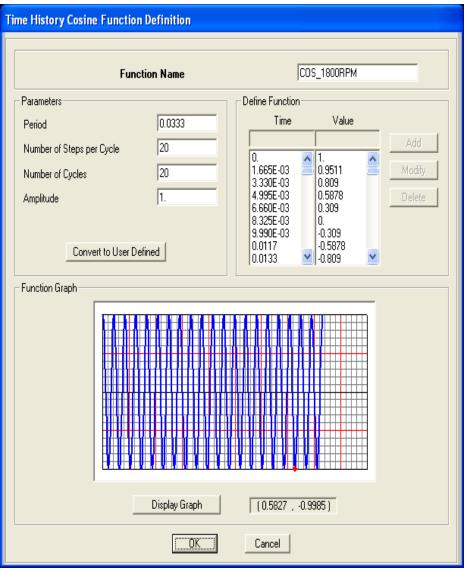


Time History Cosine Function Definition COS 1200RPM **Function Name** Define Function Parameters 4 8 1 Value Time 0.05 Period 20 Number of Steps per Cycle 20 2.500E-03 0.9511 Number of Cycles 0.809 5.000E-03 7.500E-03 0.5878 Amplitude 0.01 0.309 0.0125 0.015 -0.309-0.5878 0.0175 Convert to User Defined 0.02 -0.809 Function Graph Display Graph (0.6422 , 0.5538)

ÖK

Cancel





Define menu>Load cases, then click the 'Add New Load Case' button. Specify Load case type to be Time History as shown below, Linear "Periodic". Here we add load patterns pairing them with their associated time history functions based on machine speed. X direction load patterns are paired with Sine functions and Z direction load patterns paired with Cosine functions. The number of output steps doesn't have to exactly match the time history function when running a periodic TH, but for a transient TH analysis, the number of output time steps X time step size should be pretty close to the TH function period X number of cycles

Load Case Data - Linear Modal History	
Load Case Name Notes TH1 Set Def Name Modify/Show	Load Case Type Time History Design
Initial Conditions Zero Initial Conditions - Start from Unstressed State Continue from State at End of Modal History Important Note: Loads from this previous case are included in the current case Modal Load Case	Analysis Type C Linear C Nonlinear C Direct Integration Time History Motion Type C Transient Periodic
Loads Applied Load Type Load Name Function Scale Factor Load Patterr UNBAL_Z2 COS_1200R 1. Load Pattern UNBAL_Z1 SINE_1200RPM 1. Load Pattern UNBAL_Z1 COS_1200RPM 1. Load Pattern UNBAL_Z2 SINE_1800RPM 1. Load Pattern UNBAL_Z2 COS_1200RPM 1. Show Advanced Load Parameters	Add Modify Delete
Time Step Data Number of Output Time Steps Output Time Step Size Other Parameters	/Show

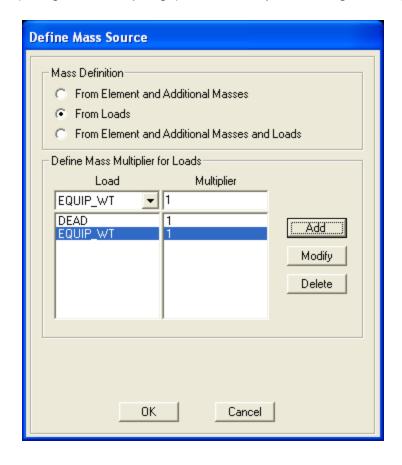
You can use the 'Add copy of load case' button to make a copy of the previous time history case and modify it to consider, for example, what would happen if one machine started out of synch from the other machine. In the case below, we use the "Advanced" load parameter to specify arrival times of loading.

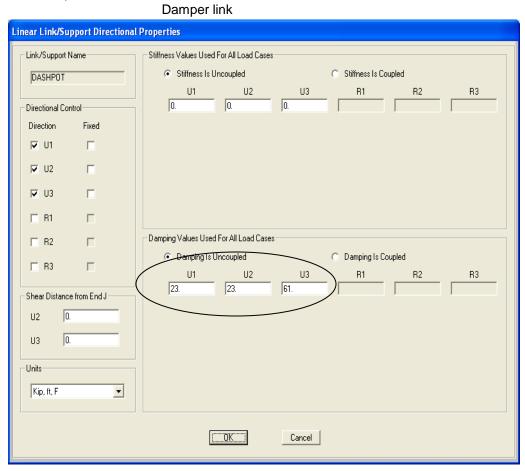
There are no limits on the number of TH cases that you can run in 1 analysis. For now, we are basing our TH analyses on Eigen Modal analysis. There is an option to use Load Dependent Ritz vectors modes instead of Eigenvectors. In larger, more complicated structures, Ritz vectors are usually more accurate for TH or response spectrum analyses, and often require more than the default 12 modes. For a small skid, it usually doesn't make much difference, so we'll use the default Eigen Modal.

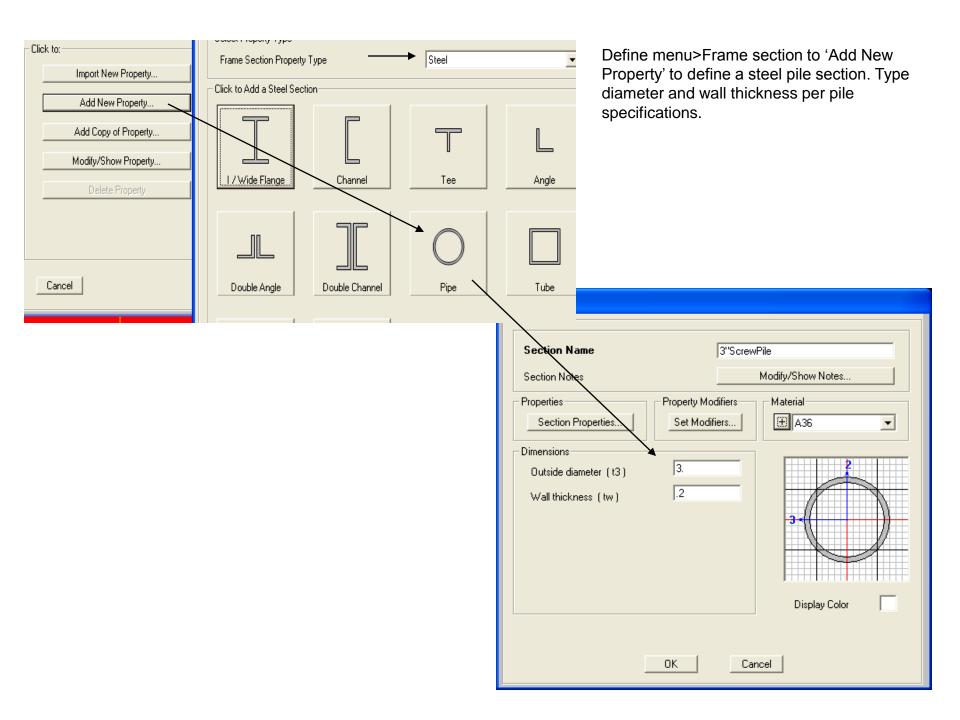
Load Case Data - Linear Modal History	
Load Case Name Notes TH-STAGGER Set Def Name Modify/Show	Load Case Type Time History Design
Initial Conditions Zero Initial Conditions - Start from Unstressed State Continue from State at End of Modal History Important Note: Loads from this previous case are included in the current case	Analysis Type C Linear C Nonlinear Time History Type C Transient C Periodic
Use Modes from Case Load Sapplied Load Type Load Name Function Scale Factor Time Factor Load Pattern UNBAL_Z ▼ COS_1201 ▼ 1. 1. Load Pattern UNBAL_Z1 UNBAL_Z1 UNBAL_Z1 UNBAL_Z1 UNBAL_Z1 UNBAL_Z1 UNBAL_Z2 SINE_1800Rf 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	
Show Advanced Load Parameters Add Time Step Data Number of Output Time Steps Output Time Step Size Add Add Output Time Steps Output Time Step Size	Modify Delete
Other Parameters Modal Damping Constant at 0.03 Modif	fy/Show Cancel

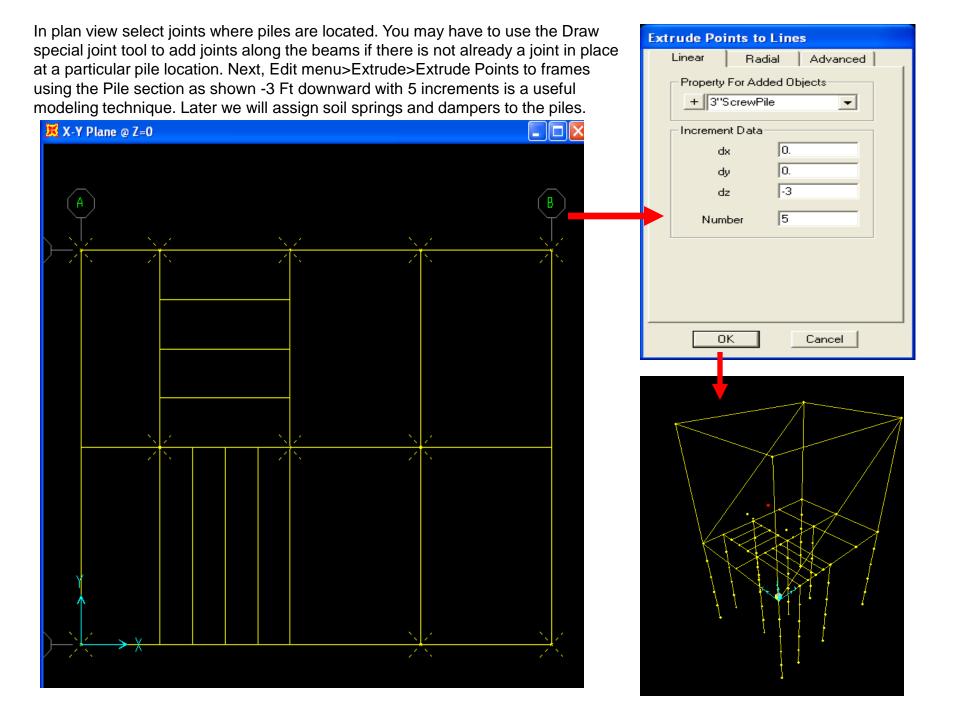
Since we assigned the vibrating machinery weight to a separate load pattern, in order to make sure it's included in the mass model use Define menu>Mass source and choose "From Loads" and add DEAD (element selfweight) and the Equipment load pattern as shown. If you had assigned other gravity loads (such as piping, cladding, stationary equipment, etc.), you would want to include them as well as part of the mass model.

Next, based on the soil report we will use Define>Section properties>Link/Support properties, choose "Linear type" to define soil damping (C) properties at selected joints in the U1, U2, and U3 local directions, which correspond to global X, Y, and Z directions. The values to be entered are the responsibility of the engineer based on soil data. Often, it's more efficient to assign the soil dampers at the pile/structure intersection joints using a link, then assign soil springs (K) using another method (Assign>Joint>Springs) at selected joints along the length of the pile.

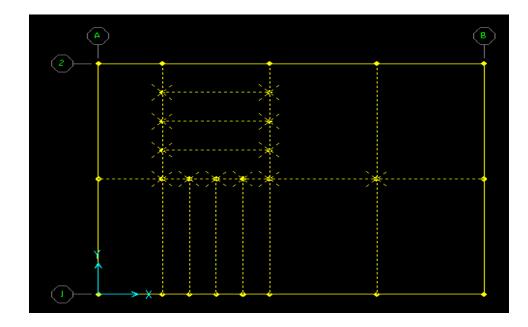


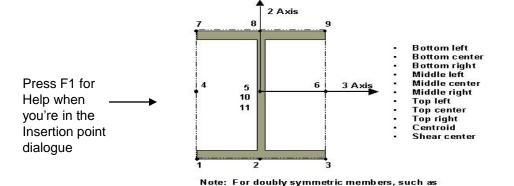




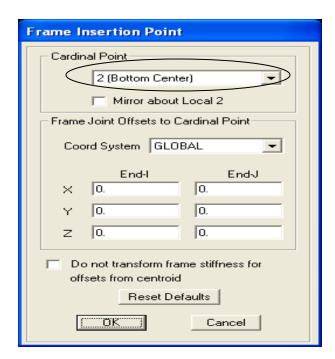


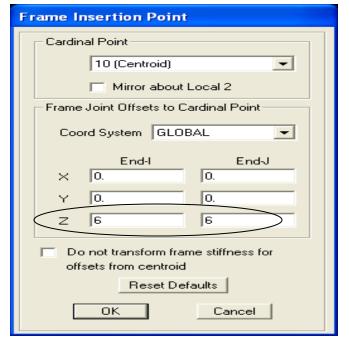
In some framing, the interior frames are connected on top of the main girders. Our default modeling assumed centerline connections, so select the interior beams and **Assign>Frame>Insertion point**. Here you can assign T.O.S and other cardinal point insertions. To the right are two options: Assign a cardinal point, or move the frame up 6", which is ½ the height of the girders. This will adjust moments based on the insertion point assignment.



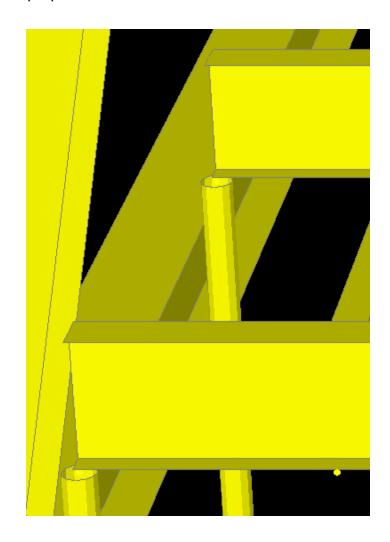


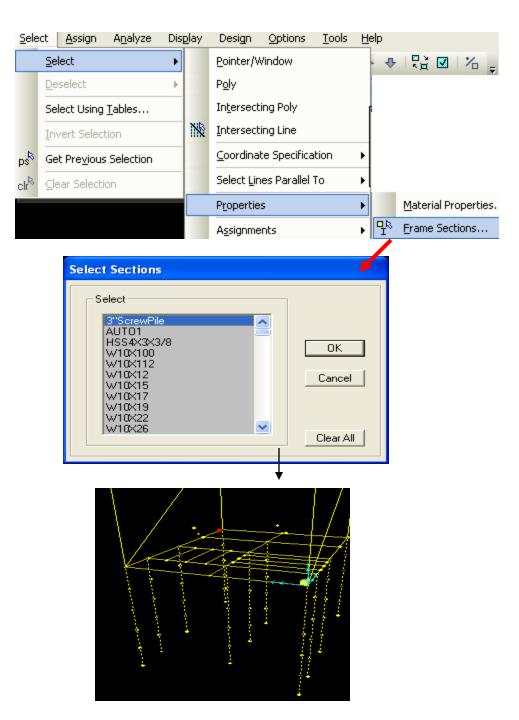
this one, central points 5, 10, and 11 are the same.



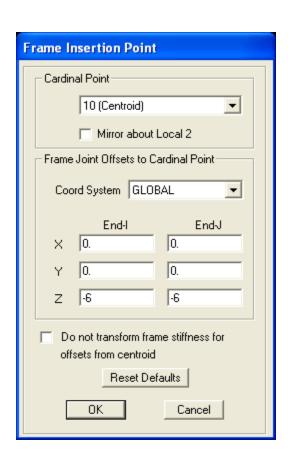


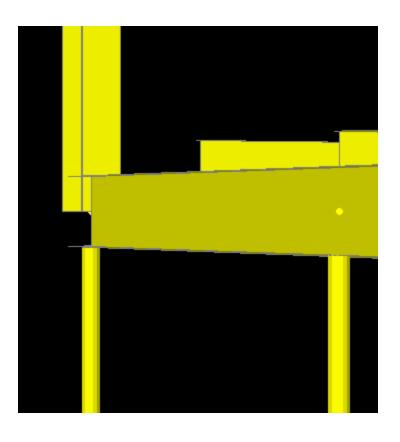
Beams on top of the girders shown using Extruded view. The pile sections need to be adjusted next. You can use Select menu as shown right and select all the piles by properties>Frame sections as shown



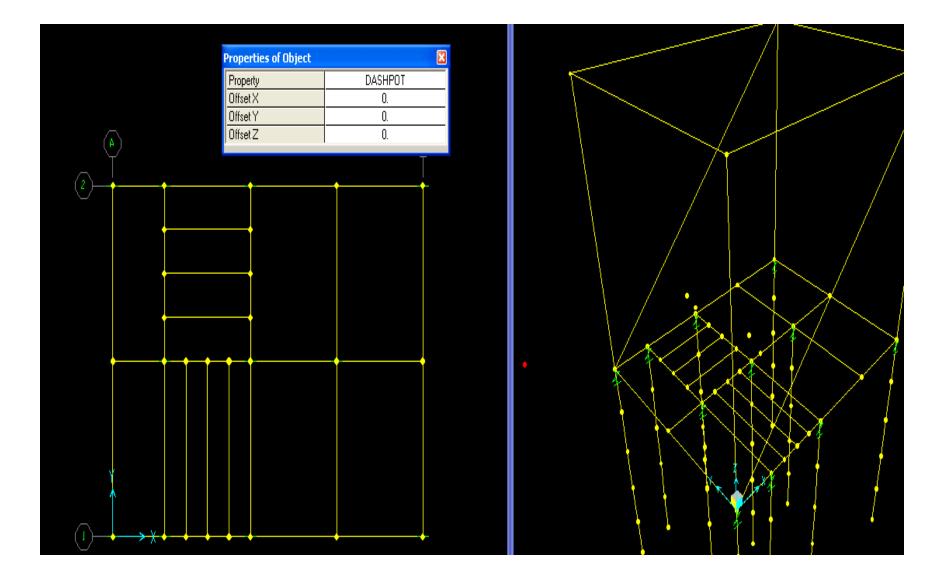


Assign>Frame>Insertion point as shown below to "move" the piles 6" in the –Z direction to connect at the bottom flange. Insertion point assignments move elements, but they are linked to the original joint location by an internal body constraint with is automatically added, and that constraint will account for moment differentials from the offsets

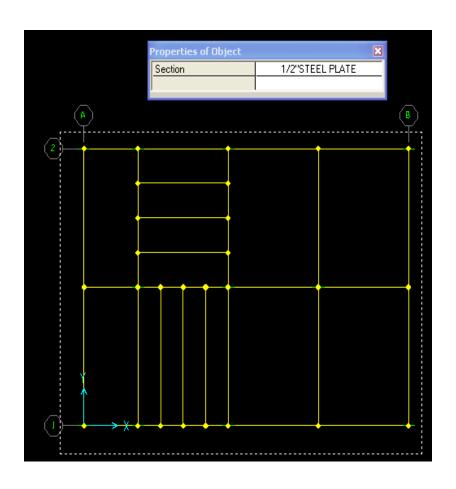


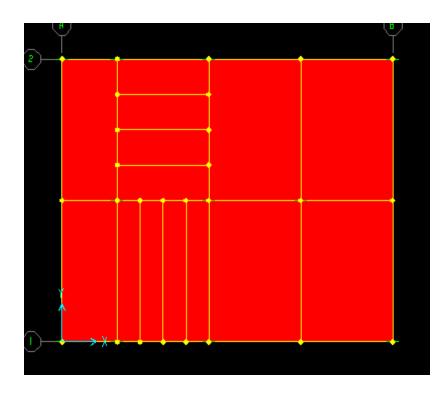


A common modeling approach is to lump the damping (C) at the joints where the pile intersects with the structure. Use Draw menu>Draw 1 joint links to add the Dashpot link. On the pile joints below, we will select them in a moment to assign lateral springs with a rotational spring component about the X.



Before adding the soil springs to the piles, we will add a steel plate to the bottom. After having used Define menu>Section properties>Area sections to predefine a steel plate section (shell), in plan view, use 'Quick draw area' to window around the area to draw the plates using the steel plate section previously defined. This adds the steel plate sections, dividing the elements at visible grid intersections, which is a start, but it's inadequate to connect to some of the interior beams, which is why we need to assign an area automesh. The nice thing about using the area automesh, is that if framing changes, the area mesh automatically changes, saving the user from having to rebuild and re-mesh sections of the model when design changes occur.

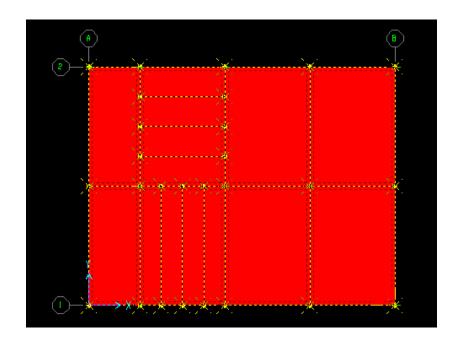




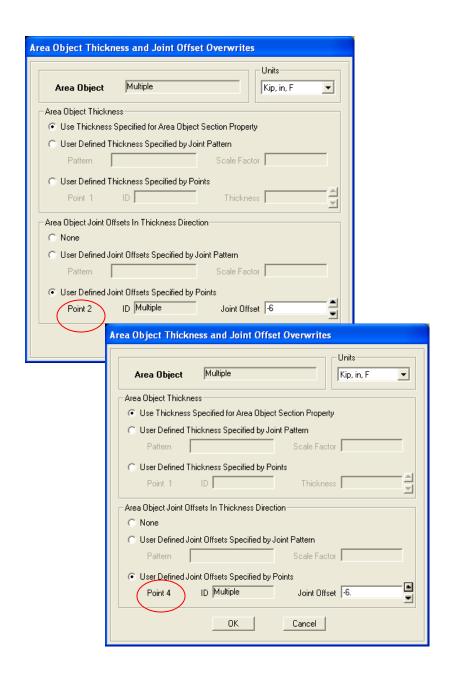
Select the steel plate/shell areas and Assign>Area>Automatic area mesh. Max size of divided element is 18" in this example. It's engineering judgment as to area mesh sensitivity. Obviously a finer mesh can take longer to run. But this automesh tool makes it easy to run sensitivity checks with different max mesh sizes

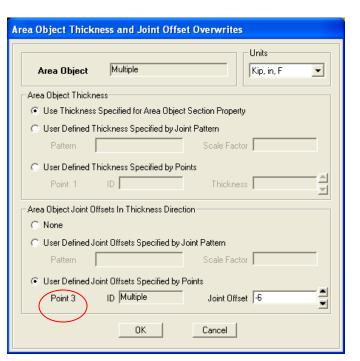
Assign Automatic Area Mesh	
No Auto Meshing Mesh Area Into This Number of Objects (Quads and Triangles Only) Along Edge from Point 1 to 2 Along Edge from Point 1 to 3	Meshing Group ALL Sub Mesh Option Sub Mesh As Required To Obtain Elements No Larger Than The Specified Maximum Size
 Mesh Area Into Objects of This Maximum Size (Quads and Triangles Only) Along Edge from Point 1 to 2 Along Edge from Point 1 to 3 Mesh Area Based On Points On Area Edges (Quads and Triangles Only) Points Determined From:	Maximum Sub Meshed Size
Local Axes For Added Points Make same on Edge if adjacent corners have same local axes definition Make same on Face if all corners have same local axes definition Restraints and Constraints For Added Points Add on Edge when restraints/constraints exist at adjacent corner points (Applies if added edge point and adjacent corner points have same local axes definition) Add on Face when restraints/constraints exist at all corner points (Applies if added face point and all corner points have same local axes definition)	OK Cancel

Since we modeled the steel plate at centerline, we'll need to "move" it to the bottom of the skid using a technique similar to the frame insertion point assignment. Select area elements then Assign>Area>Area thickness overwrites and specify, using current units (inches in this example) offsets in the local 3 normal direction, for each of 4 corners. In this example, -6 inches, ½ the depth of the girders. The screen below is Point 1. This area assignment must be repeated 3 more times for points 2, 3, and 4. See next slide.









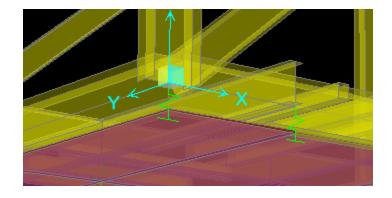
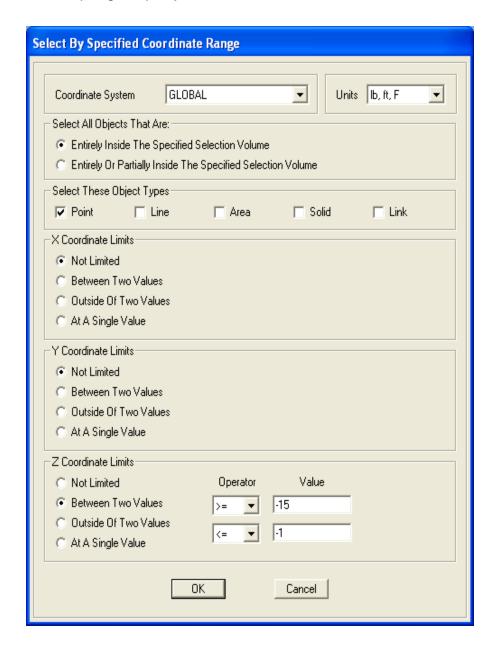
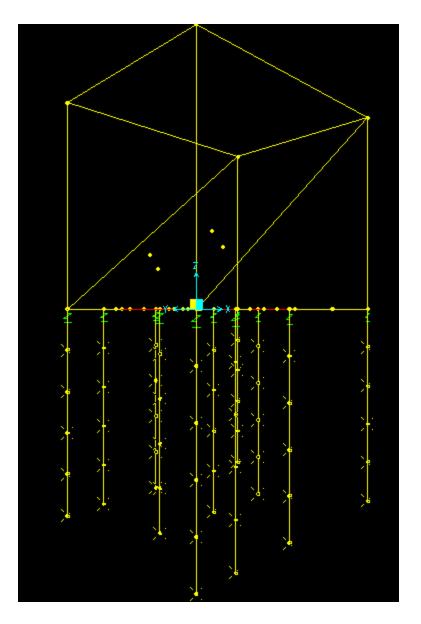


Plate at bottom of skid

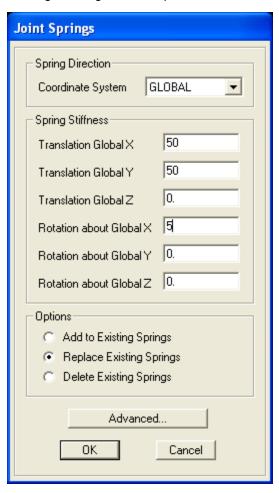
Select menu>Select>Coordinate specifications all the joints below the pile/structure intersection in order to assign soil springs at pile joint locations based on soil data



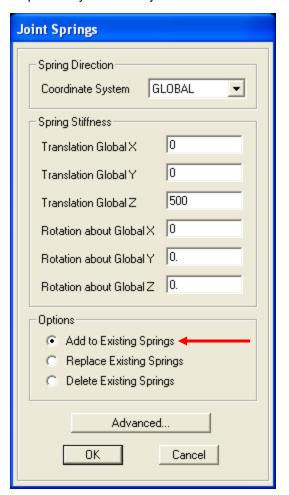


Next use Assign>Joint>Springs to assign soil joint springs along the piles. The values below are pulled out of thin air, but their ratios to each other are somewhat typical. Horizontal soil springs typically total 50% or less than vertical spring based on soil data. Often, engineers will lump the vertical spring at the bottom of the pile for dynamic analysis, while spreading the lateral soil springs at each meshed joint location along the length of the pile. A small rotational spring resisting rotations in the direction of the unbalanced loads are often assigned with the lateral springs along the length of the pile. I am not sure where engineers come up with the rotational spring values, possibly using recommendations from the book "Design of Structures and Foundations for Vibrating Machines" by Arya, O'Neill, and Pincus.

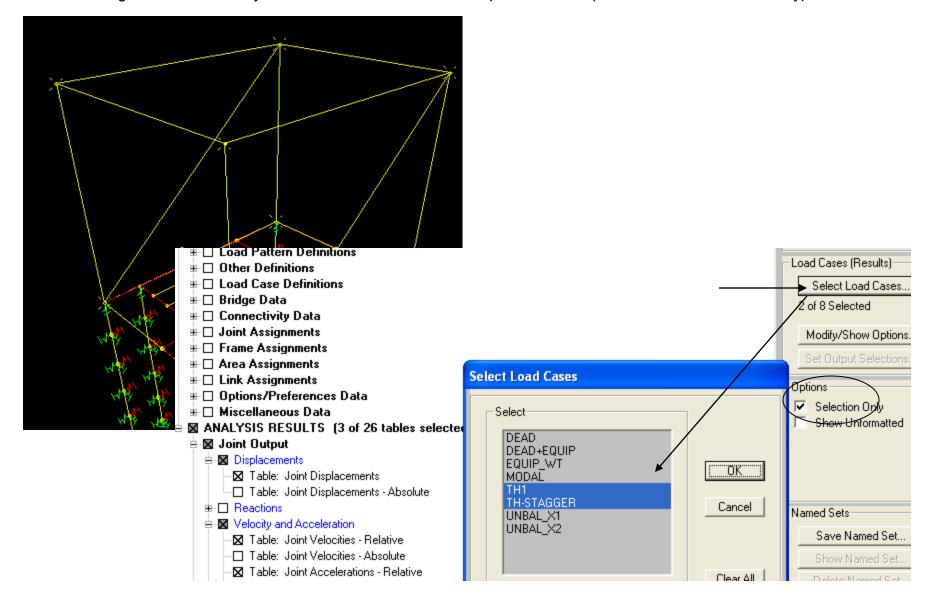
Lateral and rotational soil springs assigned to multiple joints along the length of each pile



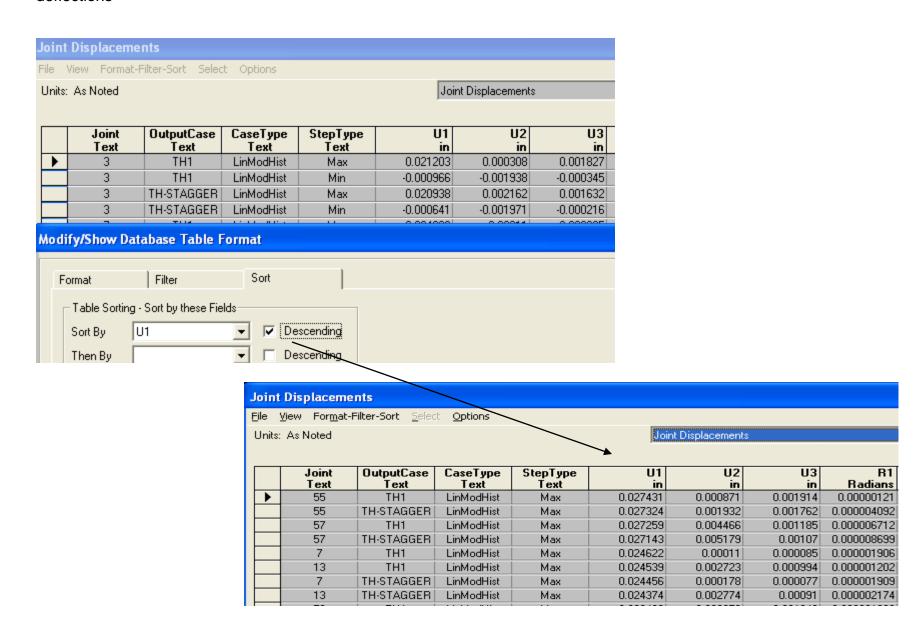
Vertical spring is often lumped at the bottom of each pile for dynamic analysis



Analyze the model and after the analysis is complete, in order to minimize output for checking deflection amplitudes, velocities, and accelerations, click to select a few joints where the highest displacements are likely to occur in order to minimize output. By selecting joints, SAP2000 will only reported results for the selected joints. Use Display menu>Show tables, but click the 'Select load cases' to generate tables only for the TH cases as shown. Output selection options shown below left are typical.



Use the Format-Filter-Sort to sort for min and max values. In the example below, sorting for max U1 (X direction) deflections





П		Joint	OutputCase	CaseType	StepType	U1	U2	U3	. R1	R2	-
Ш		Text	Text	Text	Text	in/sec	in/sec	in/sec	rad/sec	rad/sec	
	•	3	TH1	LinModHist	Max	0.2	0.05097	0.03085	0.0003432	0.000634	
		3	TH1	LinModHist	Min	-0.34	-0.03393	-0.04733	-0.0002283	-0.0009018	
		3	TH-STAGGER	LinModHist	Max	0.16	0.06188	0.02792	0.0002568	0.0005696	
		3	TH-STAGGER	LinModHist	Min	-0.3	-0.04977	-0.03483	-0.0001924	-0.0006788	
		7	TH1	LinModHist	Max	0.21	0.01097	0.02168	0.00003273	0.0002849	
		7	TH1	LinModHist	Min	-0.37	-0.01104	-0.01395	-0.00004772	-0.0002751	
		7	TH-STAGGER	LinModHist	Max	0.22	0.01805	0.01668	0.00002817	0.0002425	
		7	TH-STAGGER	LinModHist	Min	-0.32	-0.01542	-0.01166	-0.00003912	-0.0002824	
		9	TH1	LinModHist	Max	0.2	0.01104	0.009312	0.0001394	0.0003333	
		9	TH1	LinModHist	Min	-0.34	-0.01091	-0.005755	-0.0001745	-0.0005084	
		9	TH-STAGGER	LinModHist	Max	0.16	0.01815	0.008074	0.0001066	0.0002718	
		9	TH-STAGGER	LinModHist	Min	-0.3	-0.01543	-0.00517	-0.0001167	-0.0003968	
		13	TH1	LinModHist	Max	0.21	0.06818	0.09887	0.0003067	0.0006437	
		13	TH1								
		13	TH-STAGGE	DINT Accele	rations - R	elative					

TH-STAGGE File View Format-Filter-Sort Select Options

15 TH1 Units: As Noted 15 TH-STAGGE

THISTAGGE

Record:

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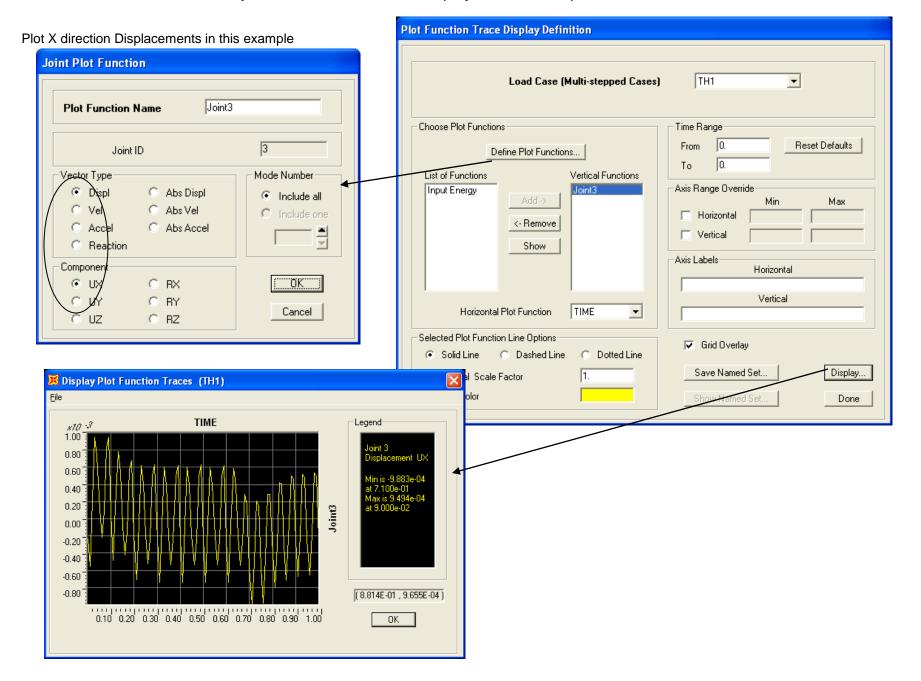
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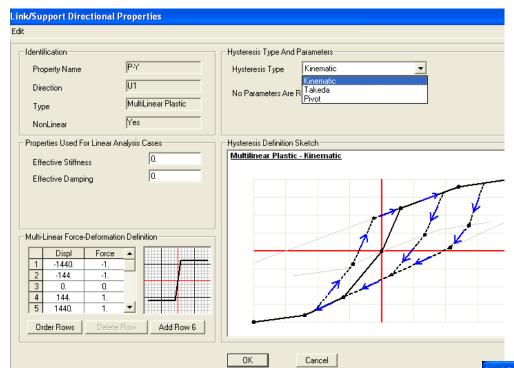
Joint Accelerations - Relative

Joint Accelerations - Relative Joint Displacements

	Joint	OutputCase	CaseType	StepType	U Join	nt Velocities - Re	lative		
: L	Text	Text	Text	Text	in/sec2	in/sec2	in/sec2	rad/sec2	rad/sec2
•	3	TH1	LinModHist	Max	19.33	6.159	2.955	0.026	0.049
•	3	TH1	LinModHist	Min	-18.514	-5.892	-4.304	-0.028	-0.078
	3	TH-STAGGER	LinModHist	Max	15.834	7.528	3.049	0.022	0.053
	3	TH-STAGGER	LinModHist	Min	-17.085	-7.565	-3.727	-0.029	-0.062
	7	TH1	LinModHist	Max	21.967	1.604	1.548	0.004601	0.015
	7	TH1	LinModHist	Min	-24.663	-1.649	-1.556	-0.003606	-0.012
	7	TH-STAGGER	LinModHist	Max	25.417	2.396	1.312	0.003429	0.011
	7	TH-STAGGER	LinModHist	Min	-25.101	-2.426	-1.665	-0.00317	-0.013
	9	TH1	LinModHist	Max	19.505	1.624	0.609	0.018	0.025
	9	TH1	LinModHist	Min	-18.623	-1.652	-0.532	-0.013	-0.038
	9	TH-STAGGER	LinModHist	Max	16.031	2.404	0.564	0.014	0.025
	9	TH-STAGGER	LinModHist	Min	-17.212	-2.45	-0.664	-0.013	-0.031
	13	TH1	LinModHist	Max	21.667	11.227	9.385	0.025	0.069
	13	TH1	LinModHist	Min	-24.391	-11.487	-7.376	-0.031	-0.086
	13	TH-STAGGER	LinModHist	Max	25,089	15 034	9.877	0.038	0.064

Click to select a joint of interest, then use Display menu>Show plot functions





Using SAP2000's multi-linear plastic link in lieu of linear springs, it's straightforward for engineers to consider nonlinear P-Y, T-Z soil data in a nonlinear TH analysis. A few changes would need to be made that are shown in the screenshots below. Ritz vectors would have to be defined and used in a NL modal TH case. Since nonlinear TH analyses do not offer the possibility of 'periodic', only a transient analysis could be performed. That's not a big deal, but the TH functions would have to be modified to increase the number of cycles. Using Ritz vectors with SAP2000's FNA nonlinear time history, run time will increase, but not by that much in many cases. I replaced 10 linear springs with plastic links in the pile/structure model, and was able to run a NL time history analysis in less than a minute.

oad Case Data - Nonlinear Modal History (FNA) Load Case Name Load Case Type TH-NL Set Def Name Modify/Show.. De Time History **-**| Initial Conditions Analysis Type Time History Zero Initial Conditions - Start from Unstressed State Nonlinea Direct Inte Transient Modal Load Case Use Modes from Case Loads Applied Load Type Load Name Function Scale Factor Load Patterr ▼ UNBAL_X1 ▼ SINE_1200F ▼ 1. Add UNBAL_Z1 UNBAL_X2 UNBAL_Z2 Load Pattern COS_1200RPM 1. SINE 1800RPM 1. Load Pattern Modify COS 1200RPM 1. Load Pattern Delete Show Advanced Load Parameters Time Step Data: Number of Output Time Steps 100 0.01 Output Time Step Size

Ritz modal includes all load patterns and Link "All" as shown

Load Case Name	Set De	4	tes Modify/Show	Load Case Type Modal
Stiffness to Use © Zero Initial Cor Stiffness at Er Important Note	nd of Nonlinear Ca	ise 	re NOT included	Type of Modes © Eigen Vectors © Ritz Vectors
	mber of Modes	,	12	
Load Type Load Pattern Link	Load Name UNBAL_Z2 DEAD UNBAL_X1 UNBAL_X2 UNBAL_Z1 UNBAL_Z1 UNBAL_Z2 All	Maximum Cycles 0 0 0 0 0 0 0 0 0	Target Dynamic Participation Ratios (%) 99 99 99 99 99 99 99 99 99	ŌK.
Ac	dd Mo	dify Del	lete	Cancel