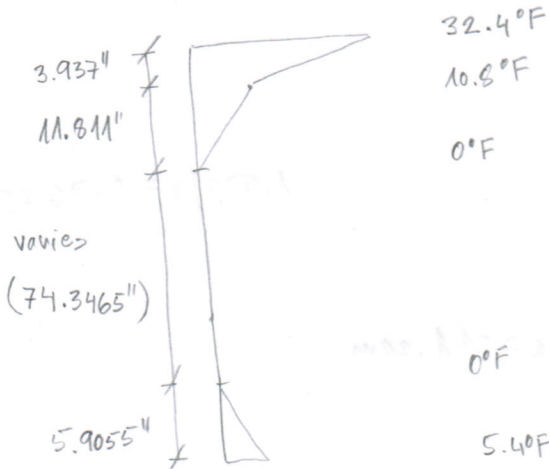
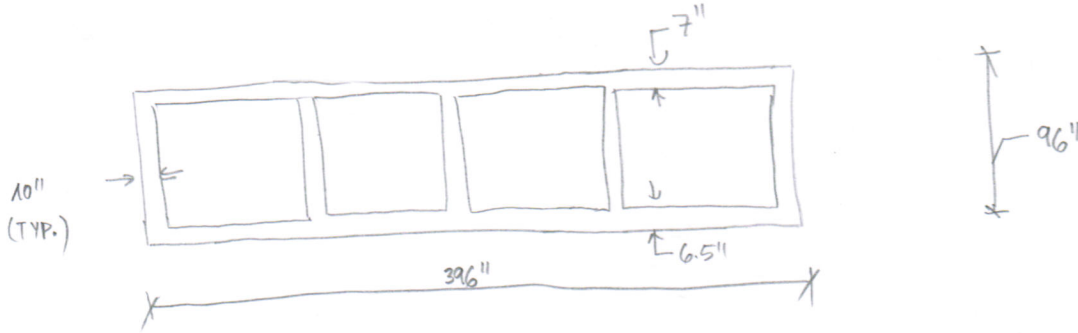


[kib, in, F]

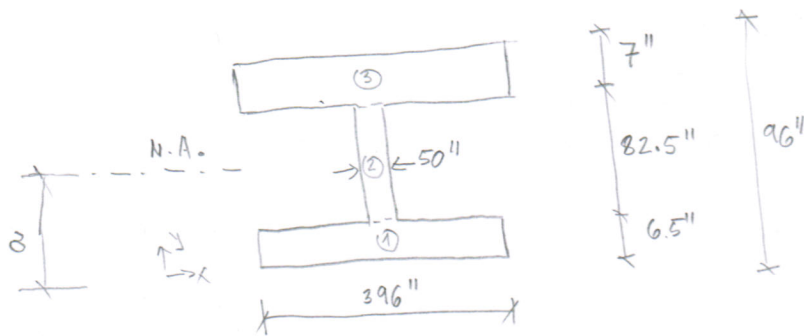
BOBJ2 > Load pattern "Temp" > Temperature gradient
BTGL1



Σ =



↓ equivalent I-section (not to scale)

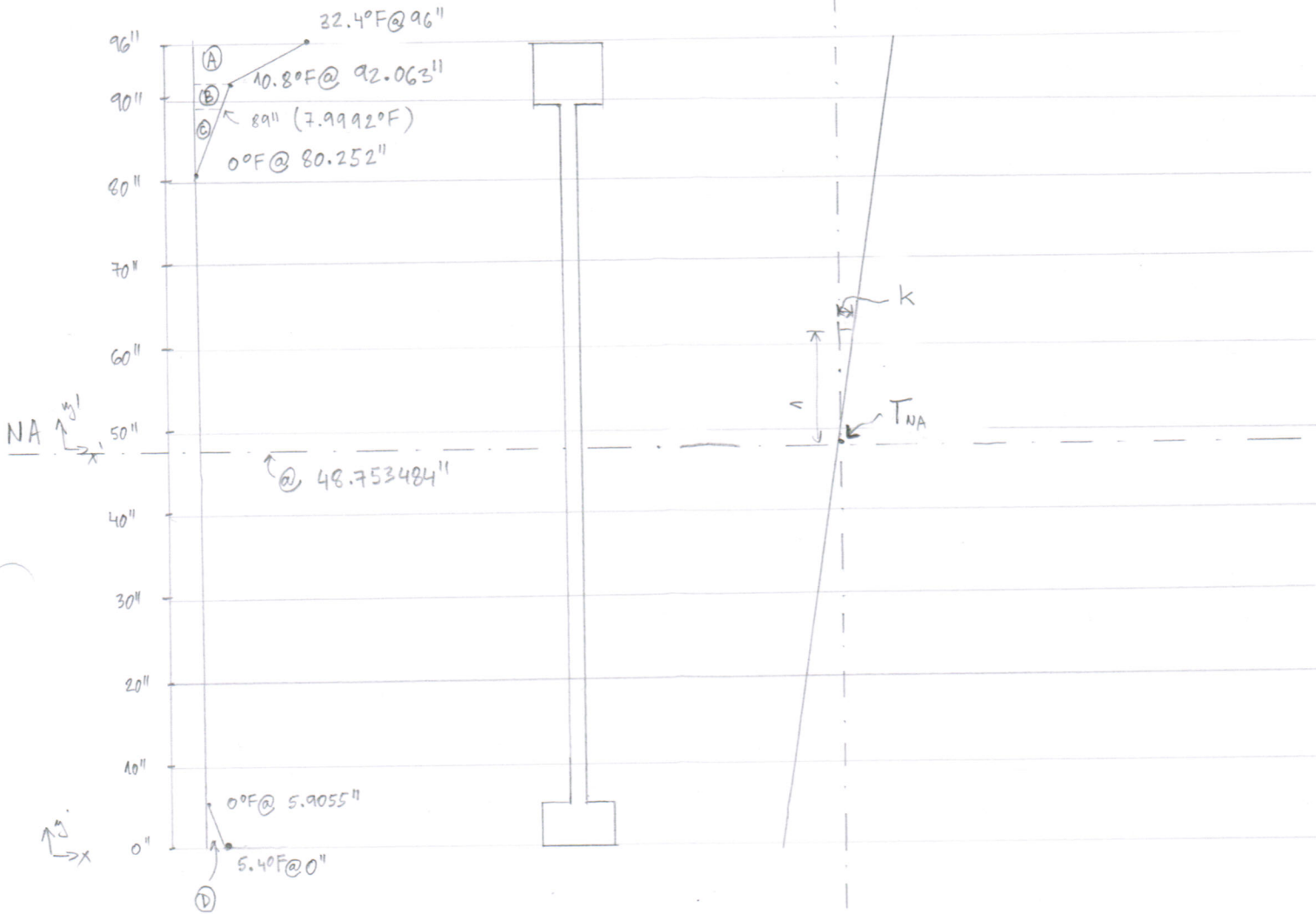


Determine a

	A	y_{cg}	$A y_{cg}$
①	2574 in ²	3.25"	8365.5
②	4125 in ²	47.75"	196968.75
③	2772 in ²	92.5"	256410
	$\Sigma = 9471 \text{ in}^2$		$\Sigma = 461744.25 \text{ in}^3$

$$a = \frac{\Sigma A y_{cg}}{\Sigma A} = 48.753484 \text{ in } \checkmark$$

Linear gradient



Subject:

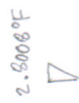
Subtask:

Prepared by: ok

Date: 7/23/2009

Sheet No. 4 of

Diagram	y _{bot}	y _{top}	Δy	section width	Integrated Temperature	y _{log}
A A ₁ A ₂	92.063"	96"	3.937"	396"	16837.7616	94.6315"
	92.063"	96"	3.937"	396"	16837.7616	94.687667"
B B ₁ B ₂	89"	92.063"	3.063"	396"	9702.613642	90.5315"
	89"	92.063"	3.063"	396"	1698.612379	91.042"
C	80.252"	89"	8.748"	50"	1749.42504	86.084"
D	0"	5.9055"	5.9055"	396"	6314.1606	1.9685"
<u>Σ 53140.33 486 (P)</u>						



+M3 \leftarrow \rightarrow +M3

Integrated Temperature
Moment

arm to NA

762 380.439

45.278016"

A1

773 428.823

45.934183"

A2

405 335.948

41.778016"

B1

71 831.797

42.288516"

B2

65 306.939

37.330516"

C

-295 407.903

-46.784984"

D

Σ 173 2896.043 (M3)

(from Excel)

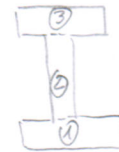
Referring to Figure on page 3 (Linear gradient), the following equations can be written (assuming $\alpha E = 1$):

$$P = \int_A T(y') dA = \int_A (T_{NA} + k y') dA = T_{NA} A + k \int_A y' dA = T_{NA} A + k Q$$

$$M_3 = \int_A y' T(y') dA = \int_A y' (T_{NA} + k y') dA = \int_A T_{NA} y' dA + \int_A k y'^2 dA = T_{NA} Q + k I$$

Where Q is static moment of Area (zero about NA)

I is moment of inertia



$$\left(\begin{array}{cc|c} T_{NA} & k & \\ \hline A & Q=0 & P \\ \hline Q=0 & I & M_3 \end{array} \right)$$

$$\begin{aligned} \text{top fiber temperature} &= 5.610847 + \\ &+ (96'' - 48.753484'') (0.137159) = 12.090^\circ\text{F} \\ \text{bottom fiber temperature} &= 5.610847 + \\ &+ (-48.753484'') (0.137159) = -1.08^\circ\text{F} \end{aligned}$$

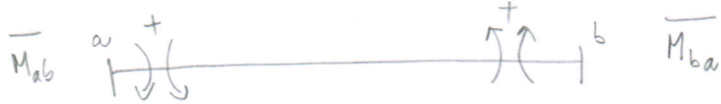
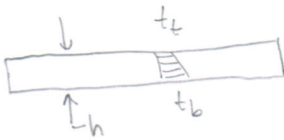
OK!

$$T_{NA} = \frac{P}{A} = \frac{53140.33486}{9471} = 5.610847^\circ\text{F}$$

$$k = \frac{M_3}{I} = \frac{1732896 \cdot 043}{12998760} = 0.137159$$

↑ from STP2000 & verified by hand

Determine fixed moments



$$\overline{M}_{ab} = \frac{EI}{h} \alpha (t_b - t_t)$$

$$\overline{M}_{ba} = -\frac{EI}{h} \alpha (t_b - t_t)$$

$$E = 3232.6008 \text{ ksi}$$

$$I = 12,998,760 \text{ in}^4$$

$$h = 96 \text{ in}$$

$$t_t = 12.09^\circ\text{F}$$

$$t_b = -1.08^\circ\text{F}$$

$$\alpha = 0.00005556 \frac{1}{^\circ\text{F}}$$

$$M = 32028.07 \text{ kip-in} \frac{1\text{ft}}{12\text{in}} =$$

$$= 2669.005 \text{ kip-ft}$$

(SAP2000 gives very similar value for single frame element and solid bridge model)