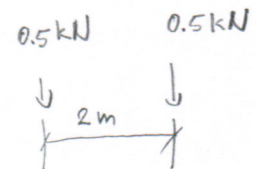
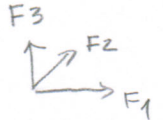


CASE AVERTICALVEHICLE ELEVATIONVEHICLE AXLE

EXPECTED REACTIONS:

$$F_1 = F_2 = 0$$

$$F_3 = 1 \text{ kN}$$

$$M_1 = (1.5 \text{ m})(0.5 \text{ kN}) = 0.75 \text{ kN-m} \quad \dots \text{ consider just 1 wheel}$$

$$M_2 = (20 \text{ m})(1 \text{ kN}) = 20 \text{ kN-m}$$

(reduction of response severity not allowed)

CENTRIFUGAL

CENTRIFUGAL LOADS

$$F_c = - \frac{v_c^2}{g} \cdot \frac{W}{R} = (-1) \frac{(20 \text{ m/s})^2}{(9.80665 \frac{\text{m}}{\text{s}^2})} \frac{(1 \text{ kN})}{(100 \text{ m})} = -0.4079 \text{ kN}$$

EXPECTED REACTIONS:

$$F_2 = 0.4079 \text{ kN}$$

$$M_1 = (0.4079 \text{ kN})(10 \text{ m}) = 4.079 \text{ kN-m}$$

$$M_1 \text{ FOR LOADS ACTING AT MID THICKNESS OF DECK} = (0.4079 \text{ kN})(9.85 \text{ m}) = 4.0178 \text{ kN-m}$$

BRAKING

$$\text{FACTOR FOR AXLE LOADS} = 0.25$$

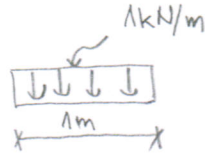
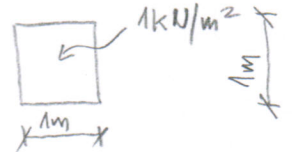
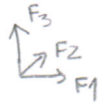
EXPECTED REACTIONS:

$$F_1 = (0.25)(1 \text{ kN}) = 0.25 \text{ kN}$$

$$M_2 = (0.25 \text{ kN})(10 \text{ m}) = 2.5 \text{ kN}$$

M_2 FOR LOADS ACTING AT MIDTHICKNESS OF

$$\text{DECK} = (0.25 \text{ kN})(9.85 \text{ m}) = 2.4625 \text{ kN-m}$$

CASE BVERTICALVEHICLE ELEVATIONVEHICLE PLAN

EXPECTED REACTIONS:

$$F_1 = F_2 = 0$$

$$F_3 = 1 \text{ kN}$$

$$M_1 = (1 \text{ kN}) (1 \text{ m}) = 1 \text{ kN-m}$$

$$M_2 = (1 \text{ kN}) (19.5 \text{ m}) = 19.5 \text{ kN-m}$$

CENTRIFUGAL

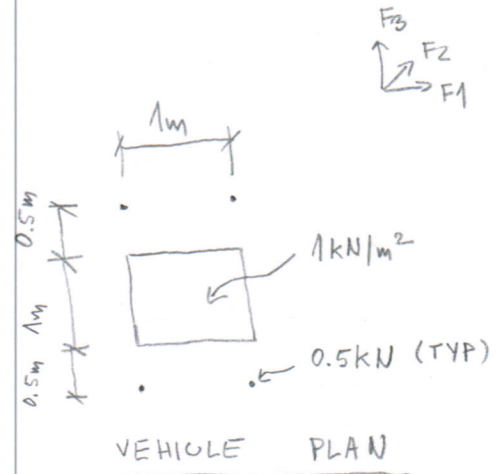
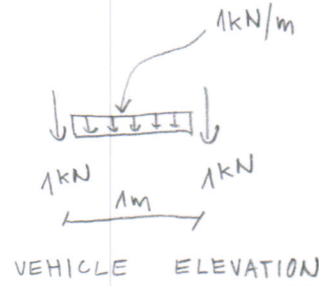
EXPECTED REACTIONS:

SAME AS FOR CASE A

BRAKING

EXPECTED REACTIONS:

SAME AS FOR CASE A

CASE CVERTICAL

NOTE:

VEHICLE LOADS (AXLE AND UNIFORM) ARE APPLIED
2m ABOVE THE DECK.

EXPECTED REACTIONS:

$$F1 = F2 = 0$$

$$F3 = 3 \text{ kN}$$

$$M1 = \underbrace{(1.5\text{m})(1\text{kN})}_{\text{Axle}} + \underbrace{(1\text{m})(1\text{kN})}_{\text{uniform at the edge of lane}} = 2.5 \text{ kN-m}$$

$$M2 = (3\text{kN})(1.5\text{m}) = 58.5 \text{ kN-m}$$

CENTRIFUGAL

USE SIMILAR CALCULATION AS FOR CASE A

EXPECTED REACTIONS:

$$F_2 = (3)(0.4079 \text{ kN}) = 1.2237 \text{ kN}$$

$$M_1 = (1.2237 \text{ kN})(10 \text{ m} + 2 \text{ m}) = 14.6844 \text{ kN-m}$$

↑ vehicle cg is 2m above the deck (note that the 2m distance is only considered when there are sufficient vertical loads to prevent overturning, which is not the case for the present model)

$$\begin{aligned} M_1' &= (1.2237 \text{ kN})(10 \text{ m} - 0.15 \text{ m}) = \\ &= 12.053 \text{ kN-m} \end{aligned}$$

BRAKING

USE SIMILAR CALCULATION AS FOR CASE A

FACTOR FOR UNIFORM AND AXLE LOADS = 0.5

EXPECTED REACTIONS:

$$F_1 = (0.5)(3 \text{ kN}) = 1.5 \text{ kN}$$

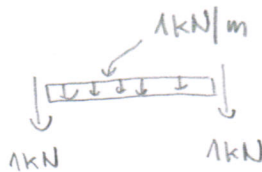
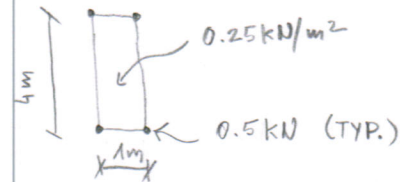
$$M_2 = (1.5 \text{ kN})(10 \text{ m} + 2 \text{ m}) = 18 \text{ kN-m}$$

↑ not considered for braking in the current implementation

$$M_2' = (1.5 \text{ kN})(10 \text{ m} - 0.15 \text{ m}) = 14.775 \text{ kN-m}$$

VERT + CENTR

10m WIDE LANE AND 4m WIDE VEHICLE HAVE BEEN USED FOR THIS LOAD CASE IN ORDER FOR THE OVERTURNING LOADS TO BE SMALLER THAN THE VERTICAL LOADS SO THAT OVERTURNING CAN BE CONSIDERED.

VEHICLE ELEVATIONVEHICLE PLAN

EXPECTED REACTIONS:

$$F_2 = 1.2237 \text{ kN} \quad (\text{SAME AS CENTRIFUGAL LOADS ONLY})$$

$$M_1 = \underbrace{(3 \text{ kN})(3 \text{ m})}_{\text{VERT. LOADS}} + \underbrace{(1.2237 \text{ kN})(9.85 \text{ m} + 2 \text{ m})}_{\text{CENTRIFUGAL LOADS}} =$$

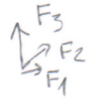
$$= 23.5006 \text{ kN-m}$$

$$F_3 = 3 \text{ kN}$$

$$F_1 = 0 \text{ kN}$$

CASE DCENTRIFUGAL

THE VEHICLE IS
THE SAME AS FOR
CASE C



CENTRIFUGAL LOADS

$$F_c = -c(L_c) \frac{W}{R} = (-1)(20m) \frac{3kN}{100m} = 0.6kN$$

EXPECTED REACTIONS

$$F_2 = 0.6kN$$

$$M_1 = (0.6kN)(10m + 2m) = 7.2kN-m$$

↑ NOT CONSIDERED DUE TO
ZERO VERTICAL LOAD

$$M_1' = (0.6kN)(10m - 0.15m) = 5.91kN-m$$